



## Inhibition of hydrogen transport through Pd and Pd<sub>47</sub>Cu<sub>53</sub> membranes by H<sub>2</sub>S at 350 °C

Casey P. O'Brien<sup>a,b</sup>, Bret H. Howard<sup>a,\*</sup>, James B. Miller<sup>a,b</sup>, Bryan D. Morreale<sup>a</sup>, Andrew J. Gellman<sup>a,b</sup>

<sup>a</sup> National Energy Technology Laboratory, US Department of Energy, P.O. Box 10940, Pittsburgh, PA 15236, United States

<sup>b</sup> Department of Chemical Engineering, Carnegie Mellon University, Pittsburgh, PA 15213, United States

### ARTICLE INFO

#### Article history:

Received 11 June 2009

Received in revised form 2 November 2009

Accepted 30 November 2009

Available online 4 December 2009

#### Keywords:

Palladium–copper membrane

Hydrogen sulfide

Palladium sulfide

Sulfur poisoning

### ABSTRACT

In pure H<sub>2</sub> gas, hydrogen fluxes through pure Pd and Pd<sub>47</sub>Cu<sub>53</sub> (mol%) foils at 350 °C are similar. In the presence of 1000 ppm H<sub>2</sub>S in H<sub>2</sub>, the hydrogen fluxes through both foils are substantially reduced, but with significantly different decay patterns. Six hours after the start of H<sub>2</sub>S exposure, the Pd foil remained permeable to hydrogen, with the flux decreasing slowly over time. Analysis of the Pd foil by X-ray diffraction (XRD) and scanning electron microscopy (SEM) reveals that Pd reacts with H<sub>2</sub>S to form a palladium sulfide corrosion product, Pd<sub>4</sub>S, which is about 6.6 μm thick. These observations are consistent with the slow growth of a low-permeability, but catalytically active, sulfide corrosion layer on the Pd surface. In contrast, the hydrogen flux through the Pd<sub>47</sub>Cu<sub>53</sub> foil is undetectable within 5 min of the start of H<sub>2</sub>S exposure. XPS depth profiling of the Pd<sub>47</sub>Cu<sub>53</sub> foil reveals that sulfur penetrates only ~3 nm into the Pd<sub>47</sub>Cu<sub>53</sub> surface. Rapid formation of a Pd–Cu–S terminal layer, which is either inactive for hydrogen dissociation or impermeable to hydrogen atoms, is responsible for the deactivation of the Pd<sub>47</sub>Cu<sub>53</sub> alloy membrane in H<sub>2</sub>S at 350 °C.

© 2010 Published by Elsevier B.V.

### 1. Introduction

State-of-the-art gasification processes are being developed to reduce both foreign oil dependence and greenhouse gas emissions. Coal will be a primary fuel source for these processes and will produce a variety of secondary energy products including hydrogen, liquid fuels, and electricity with near-zero greenhouse gas emissions. Generating hydrogen from coal presents significant technical challenges, including the need to separate hydrogen from mixed gas streams composed primarily of H<sub>2</sub> and CO<sub>2</sub> with several minor constituents such as steam, CO, and H<sub>2</sub>S.

Dense metal membranes are promising candidates for H<sub>2</sub>/CO<sub>2</sub> separation due in part to their potential to produce high purity hydrogen and a high pressure CO<sub>2</sub>-rich stream that is amenable to sequestration. Hydrogen permeates through metal membranes by means of a unique mechanism in which H<sub>2</sub> dissociatively adsorbs on the catalytically active surface of the metal, producing hydrogen atoms which diffuse through the interstices of the bulk metal lattice and recombine on the opposite surface. Only hydrogen atoms are able to diffuse through the bulk metal and an infinite selectivity for H<sub>2</sub> separation can be achieved. For sufficiently thick membranes with sufficiently high H<sub>2</sub> dissociation rates on the surface,

hydrogen atom diffusion through the bulk limits the overall rate of hydrogen transport [1–10]. The performance of Pd membranes is distinguished from other pure metal membranes by the high H<sub>2</sub> dissociation activity of the Pd surface and the high hydrogen atom permeability of bulk Pd [11]. However, H<sub>2</sub>S concentrations as low as parts-per-million (ppm) can severely corrode pure Pd membranes, compromising both the mechanical strength and high hydrogen permeability of the membrane [2,12–18].

To impart resistance to corrosion by H<sub>2</sub>S, Pd has been alloyed with other metals [2,13,15,17,18]. Hydrogen transport through Pd–Cu alloys has received significant attention from both experimental and computational researchers [2–4,13,15–34]. The Pd<sub>47</sub>Cu<sub>53</sub> (mol%) alloy has the highest hydrogen permeability at 350 °C among the Pd–Cu alloys [4,22,25,26], and is comparable in its hydrogen permeability to pure Pd at the same temperature. At higher temperatures (635 °C), hydrogen transport through Pd<sub>47</sub>Cu<sub>53</sub> is not significantly inhibited by 1000 ppm H<sub>2</sub>S [29]. At 350 °C, however, hydrogen transport through Pd<sub>47</sub>Cu<sub>53</sub> is severely inhibited by H<sub>2</sub>S [13,15,16,29]. In this report, we contrast the responses of Pd and Pd<sub>47</sub>Cu<sub>53</sub> membranes to exposure to 1000 ppm H<sub>2</sub>S at 350 °C. We analyze the compositions of the S-contaminated membranes by X-ray diffraction and X-ray photoelectron spectroscopy depth profiles to provide a framework for understanding the differences in their H<sub>2</sub>S-induced performance degradation. This work shows that the pure Pd foil corrodes to form a thick (~μm) Pd<sub>4</sub>S layer that retains some ability to dissociate and transport hydrogen. In contrast, the Pd<sub>47</sub>Cu<sub>53</sub> alloy foil forms a very

\* Corresponding author. Tel.: +1 412 386 5908; fax: +1 412 386 5920.  
E-mail address: [bret.howard@netl.doe.gov](mailto:bret.howard@netl.doe.gov) (B.H. Howard).

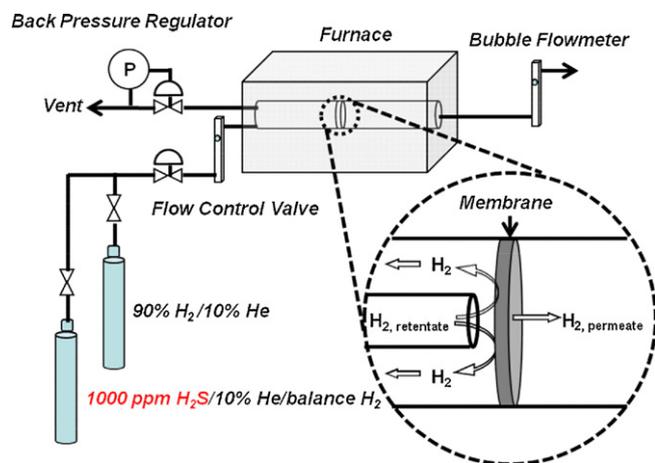


Fig. 1. Schematic of the membrane testing apparatus.

thin ( $\sim$ nm) Pd–Cu–S layer that is completely impermeable to hydrogen.

## 2. Experimental

Hydrogen transport measurements were performed using foil membranes of pure Pd and Pd<sub>47</sub>Cu<sub>53</sub>. Circular membrane foils were cut from 25  $\mu$ m thick Pd (Alfa Aesar, 99.9% metals purity) and 25  $\mu$ m thick Pd<sub>47</sub>Cu<sub>53</sub> (ATI Wah Chang, 99.0% metals purity) foils. The membranes were washed with acetone and mounted into a Swagelok® VCR tube assembly. The effective membrane surface area was about 1.8 cm<sup>2</sup>. Membranes were leak-tested by pressurizing the retentate (upstream) side of the membranes with 300 kPa of Ar and observing the pressure for 20 min. A leak-proof membrane was indicated by less than 1 kPa pressure drop on the upstream side. The leak-tested membrane tube assembly was then installed in the membrane testing apparatus which is shown schematically in Fig. 1.

Prior to making hydrogen permeation measurements, the membranes were heated to 350 °C in He (retentate, upstream) and Ar (permeate, downstream). Then the retentate sides of the membranes were exposed to a flowing mixture of 90% H<sub>2</sub>/10% He (Butler Gas Products, Inc.) at 310 kPa, with the permeated H<sub>2</sub> collected

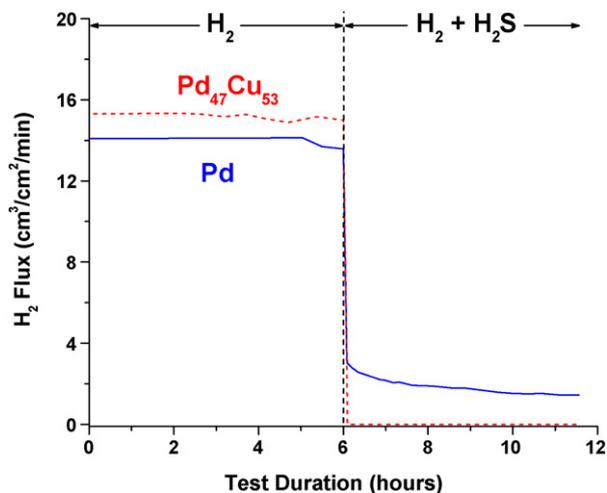


Fig. 2. Hydrogen flux through 25  $\mu$ m Pd (blue solid line) and Pd<sub>47</sub>Cu<sub>53</sub> (red dashed line) membranes versus test duration at 350 °C, total retentate pressure of 310 kPa and total permeate pressure of  $\sim$ 100 kPa (ambient pressure). A 90% H<sub>2</sub>/10% He mixture was exposed to the membrane surface during the first portion of the test and then 1000 ppm H<sub>2</sub>S/10% He/balance H<sub>2</sub> was fed to the membrane surface at 6 h.

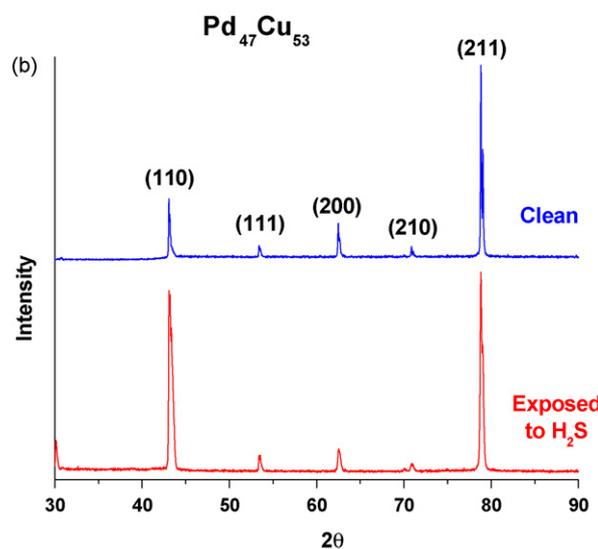
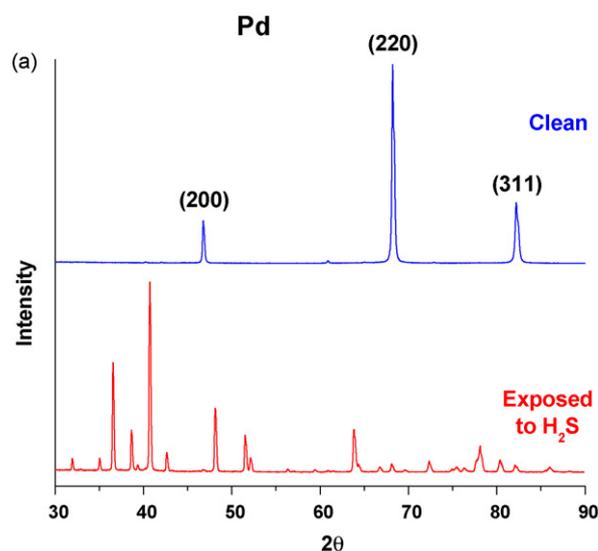
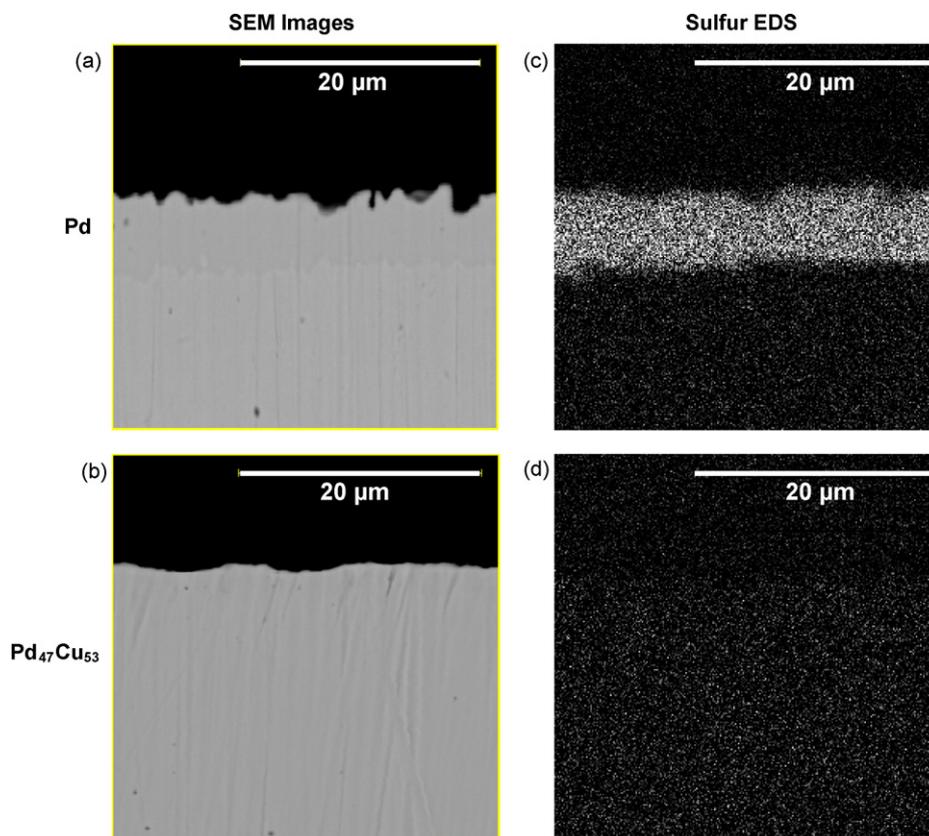


Fig. 3. X-ray diffraction patterns of (a) 25  $\mu$ m Pd foil before (clean) and after exposure to 1000 ppm H<sub>2</sub>S for 6 h (exposed to H<sub>2</sub>S) and (b) 25  $\mu$ m Pd<sub>47</sub>Cu<sub>53</sub> foil before (clean) and after exposure to 1000 ppm H<sub>2</sub>S for 6 h (exposed to H<sub>2</sub>S).

at ambient pressure ( $\sim$ 100 kPa). The temperature was measured using Omega type-K thermocouples positioned  $\sim$ 5 mm from the surface of each side of the membrane; the operating temperature was given by the average of the two temperatures. The H<sub>2</sub> flux through the membrane was measured using a bubble flowmeter (Alltech Digital Flowmeter Model 4074). A 1000 ppm H<sub>2</sub>S/10% He/balance H<sub>2</sub> mixture (Butler Gas Products, Inc.) was introduced to the membrane surface following the 90% H<sub>2</sub>/10% He mixture. The permeate gas composition was periodically analyzed by a gas chromatograph (Agilent Technologies Model 6890N) for its He content in order to confirm the absence of pinholes in the membrane. No He was detected in the permeate stream during the entire duration of the membrane tests, both before and during H<sub>2</sub>S exposure. Following data collection, the membranes were cooled to room temperature in He and Ar and then dismantled for characterization.

X-ray diffraction (XRD) measurements of the foil surfaces were obtained using a PANalytical X'Pert Pro MPD powder diffractometer having a theta–theta configuration, a Cu X-ray source operated at 45 kV and 40 mA and an X'Celerator detector equipped with a monochromator. Patterns were recorded over a  $2\theta$  range of 30–90°



**Fig. 4.** Scanning electron micrographs of cross-sections of the (a) Pd and (b) Pd<sub>47</sub>Cu<sub>53</sub> foils that were exposed to H<sub>2</sub>S for 6 h. Sulfur X-ray mapping in the SEM images of the (c) Pd and (d) Pd<sub>47</sub>Cu<sub>53</sub> cross-sections highlight the S-rich regions in white.

at a step size of 0.02°. Foil samples were mounted on zero background quartz slides for analysis. Sample foils were not perfectly flat resulting in a slight peak shape distortion; however this distortion did not affect data interpretation.

Scanning electron microscope (SEM) analysis of cross-sections of the foils was performed to determine the nature of the films grown on their surface during exposure to H<sub>2</sub>S. Cross-sectioned pieces of the Pd and Pd<sub>47</sub>Cu<sub>53</sub> foils were set in epoxy and then polished with Carbimet Paper (Buehler) up to 1200 grit. The polished cross-sections were then analyzed with an Aspex Personal SEM 2000 which was operated with a 20 keV electron beam. Sulfur X-ray maps of the cross-sections were used to quantify the thickness of the surface sulfide formed on the membrane foils.

X-ray photoelectron spectroscopy (XPS) measurements were used to determine the surface compositions of the foils and for depth profiling of the composition in the near-surface region. XPS measurements were performed on a PHI 5600ci instrument. The XPS instrument employed monochromatic aluminum K<sub>α</sub> X-rays and the pass energy of the analyzer was 58.7 eV. Elemental surface concentrations were calculated from Cu 2p<sub>3/2</sub>, Pd 3d<sub>5/2</sub>, and S 2p<sub>3/2</sub> peak areas and calibrated sensitivity factors. Depth profiles of elemental composition were acquired using Ar<sup>+</sup> as the sputtering gas and XPS analysis of surface composition. The differentially pumped ion gun was operated at 1.5 × 10<sup>-2</sup> Pa and 25 mA, producing a sputtering rate of approximately 10 nm/min based on calibration against the sputter rate of a 10 nm Pt film.

### 3. Results and discussion

Hydrogen fluxes through Pd and Pd<sub>47</sub>Cu<sub>53</sub> membranes were measured, first in the absence of H<sub>2</sub>S to establish a baseline, and then in the presence of 1000 ppm H<sub>2</sub>S. Results of the membrane test are presented in Fig. 2. Baseline hydro-

gen fluxes through the two foils were ~14 cm<sup>3</sup>/cm<sup>2</sup>/min for Pd and ~15 cm<sup>3</sup>/cm<sup>2</sup>/min for Pd<sub>47</sub>Cu<sub>53</sub>. Assuming Sievert's Law is obeyed, the calculated H<sub>2</sub> permeabilities from the baseline H<sub>2</sub> fluxes were ~1.3 × 10<sup>-8</sup> mol/m/s/Pa<sup>1/2</sup> for Pd<sub>47</sub>Cu<sub>53</sub> and ~1.2 × 10<sup>-8</sup> mol/m/s/Pa<sup>1/2</sup> for Pd; both are in good agreement with published permeability values [25,35]. The fact that these are so similar is expected; at 350 °C, the hydrogen permeability of body-centered-cubic Pd<sub>47</sub>Cu<sub>53</sub> is known to be similar to that of the face-centered-cubic Pd [13,20,21,25]. Both membranes displayed significant decreases in hydrogen flux upon exposure to 1000 ppm H<sub>2</sub>S. The hydrogen flux through the Pd<sub>47</sub>Cu<sub>53</sub> foil was below the detection limit of the bubble flowmeter (<~0.06 cm<sup>3</sup>/cm<sup>2</sup>/min) within 5 min of H<sub>2</sub>S exposure. In contrast, after an initially rapid decline, the hydrogen flux through the Pd foil slowed significantly. After 6 h of H<sub>2</sub>S exposure, the hydrogen flux through the Pd membrane was still 10% of its baseline value.

To determine whether any thick metal-sulfide compounds (corrosion layers) formed as a result of H<sub>2</sub>S exposure, the Pd and Pd<sub>47</sub>Cu<sub>53</sub> foils were analyzed by X-ray diffraction (XRD) following membrane testing. Fig. 3(a) and (b) display the XRD patterns for the Pd and Pd<sub>47</sub>Cu<sub>53</sub> foils, respectively, including diffraction patterns of the clean Pd and Pd<sub>47</sub>Cu<sub>53</sub> foils for reference. As expected, the diffraction pattern of the clean Pd foil exhibits features that are assignable to the face-centered-cubic Pd structure. The XRD pattern of the Pd foil that was exposed to H<sub>2</sub>S is dominated by features that can be assigned to crystalline palladium sulfide (Pd<sub>4</sub>S), with only very small peaks from metallic Pd. These results illustrate that H<sub>2</sub>S exposure causes the Pd membrane to form a specific palladium sulfide reaction product, Pd<sub>4</sub>S; we have described the mechanism of this reaction in previous reports [12,13,18]. In contrast to the XRD results from the Pd foil, the XRD patterns of the clean Pd<sub>47</sub>Cu<sub>53</sub> foil and the Pd<sub>47</sub>Cu<sub>53</sub> foil after 6 h of H<sub>2</sub>S exposure (Fig. 3(b)) are nearly identical and are both assignable to the

body-centered-cubic structure of Pd<sub>47</sub>Cu<sub>53</sub>. The diffraction peak intensities of the clean and H<sub>2</sub>S-exposed Pd<sub>47</sub>Cu<sub>53</sub> foils are not identical and vary from the intensities expected for an ideal body-centered-cubic Pd<sub>47</sub>Cu<sub>53</sub> powdered sample. The peak intensities observed for the clean Pd foil also vary from the intensities expected for an ideal face-centered-cubic Pd powdered sample. These variations are probably due to the fact that non-ideal solid metal foil samples were analyzed. The discrepancies in peak intensity probably reflect a preferred orientation of the metal crystallites comprising the membrane foils.

Cross-sections of the Pd and Pd<sub>47</sub>Cu<sub>53</sub> foils were imaged by SEM to determine the thickness of sulfur corrosion layers on the surface of the foils. The sulfur concentration was mapped over the SEM images by EDS. SEM analysis of the Pd and Pd<sub>47</sub>Cu<sub>53</sub> foils after H<sub>2</sub>S exposure are presented in Fig. 4(a) and (b), respectively; EDS mapping of sulfur concentration in the SEM images of the Pd and Pd<sub>47</sub>Cu<sub>53</sub> foils are presented in Fig. 4(c) and (d), respectively. A noticeable difference in the roughness of the Pd and Pd<sub>47</sub>Cu<sub>53</sub> foil surfaces exposed to H<sub>2</sub>S is evident from the SEM images in Fig. 4; the surface of the Pd foil (Fig. 4(a)) is significantly rougher than that of the Pd<sub>47</sub>Cu<sub>53</sub> foil (Fig. 4(b)). Sulfidation of the Pd foil surface to Pd<sub>4</sub>S is probably responsible for the fact that the Pd foil surface is rougher than that of the Pd<sub>47</sub>Cu<sub>53</sub> foil, which did not form any sulfur compounds that could be detected by XRD. EDS reveals a sulfur-rich layer on the surface of the Pd foil (Fig. 4(c)), which XRD identified as a Pd<sub>4</sub>S film, that is  $\sim 6.6 \pm 0.9 \mu\text{m}$  thick (average of 75 different thickness measurements across the entire length of the Pd foil cross-section). In contrast to the sulfur film observed on the Pd foil, EDS (Fig. 4(d)) did not detect a significant amount of sulfur on the Pd<sub>47</sub>Cu<sub>53</sub> foil after H<sub>2</sub>S exposure. EDS analyzes X-rays from a relatively large volume within the sample, however, and thus it is not able to detect sulfur contamination in a very thin layer near the surface of the Pd<sub>47</sub>Cu<sub>53</sub> membrane.

XPS depth profiles of the Pd and Pd<sub>47</sub>Cu<sub>53</sub> foils were collected to detect sulfur contamination near the membrane surfaces that may be undetectable by XRD and EDS analysis. XPS composition depth profiles of the Pd and Pd<sub>47</sub>Cu<sub>53</sub> foils after 6 h of H<sub>2</sub>S exposure are presented in Fig. 5(a) and (b), respectively. The Pd foil (Fig. 5(a)) has a stoichiometry in the near-surface region ( $\sim 200$  nm) that is approximately constant at Pd:S  $\approx$  4:1, which is consistent with the presence of Pd<sub>4</sub>S as indicated by the XRD results. In contrast, S appears only very near the top-surface of the Pd<sub>47</sub>Cu<sub>53</sub> alloy membrane (Fig. 5(b)); its signal decayed to zero after Ar<sup>+</sup> sputtering only  $\sim 3$  nm into the bulk of the Pd<sub>47</sub>Cu<sub>53</sub> membrane.

Pd and Pd<sub>47</sub>Cu<sub>53</sub> membranes clearly respond differently to H<sub>2</sub>S exposure at 350 °C. We believe that the different responses in hydrogen flux to H<sub>2</sub>S exposure exhibited by the two membranes are related to the evolution of their surface compositions during H<sub>2</sub>S exposure. Furthermore, two different mechanisms may be responsible for the inhibition of hydrogen transport through the two membranes: poisoning of the catalytic dissociation of H<sub>2</sub> at the surface and reduced permeability of hydrogen through the bulk of the membrane.

The observation of non-zero flux through the Pd foil during H<sub>2</sub>S exposure indicates that the membrane surface retained H<sub>2</sub> dissociation activity. The continuous slow decline of the hydrogen flux through the Pd membrane is indicative of an increasing resistance to hydrogen transport, which is consistent with hydrogen atom diffusion being retarded by a slowly thickening, dense, low-permeability Pd<sub>4</sub>S corrosion layer on the surface. This mechanism has been suggested by Morreale et al. who estimated the hydrogen permeability of Pd<sub>4</sub>S at 350 °C to be  $\sim 1/20$ th that of Pd by correlating Pd<sub>4</sub>S growth kinetics to the decline in hydrogen flux through a Pd membrane during H<sub>2</sub>S exposure [12,13]. The steep initial decline in hydrogen flux through the Pd membrane immediately following H<sub>2</sub>S exposure may be due to a rapid initial corrosion rate that slows

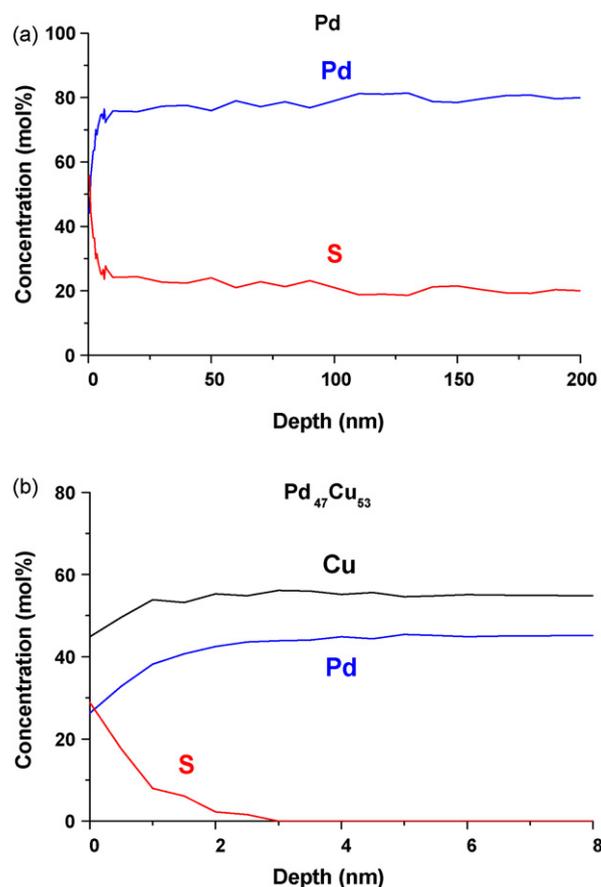


Fig. 5. X-ray photoelectron spectroscopy depth profiles of the (a) 25  $\mu\text{m}$  Pd and (b) 25  $\mu\text{m}$  Pd<sub>47</sub>Cu<sub>53</sub> membranes exposed to 1000 ppm H<sub>2</sub>S for 6 h. Elemental concentrations shown for Pd (blue), S (red), and Cu (black). The sputtering rate is  $\sim 10$  nm/min as measured using a pure Pt film. (For interpretation of the references to color in this figure caption, the reader is referred to the web version of the article.)

as diffusion of Pd and/or S ions through the Pd<sub>4</sub>S scale becomes slower. Another possible explanation for the rapid initial decline in hydrogen flux through the Pd membrane following H<sub>2</sub>S exposure is that the catalytic activity of the Pd<sub>4</sub>S surface may be significantly lower than that of Pd. As the thickness of the low-permeability Pd<sub>4</sub>S film grows beyond a critical value, hydrogen atom diffusion through the bulk becomes rate limiting. A third explanation for the evolution of the hydrogen flux is that there may be a significant barrier to hydrogen atom transport across the Pd<sub>4</sub>S/Pd interface that dominates transport initially but becomes insignificant as the Pd<sub>4</sub>S thickness grows beyond a critical value.

The immediate decline in hydrogen flux through the Pd<sub>47</sub>Cu<sub>53</sub> membrane at the start of H<sub>2</sub>S exposure must be related to the properties of its thin Pd–Cu–S terminal layer. Neither XRD nor XPS depth profiling could identify this thin Pd–Cu–S terminal layer as a specific compound and, therefore, the mechanism of its formation is not clear. Presumably this layer is either inactive for hydrogen dissociation (“sulfur-poisoned”) or it displays near-zero hydrogen atom permeability.

#### 4. Conclusions

As expected, hydrogen fluxes through 25  $\mu\text{m}$  Pd and Pd<sub>47</sub>Cu<sub>53</sub> membranes at 350 °C were observed to be comparable in the absence of H<sub>2</sub>S in the hydrogen feed. However, their interactions with H<sub>2</sub>S, and the resulting effects of H<sub>2</sub>S on hydrogen flux, were significantly different. Six hours of exposure of the Pd foil to 1000 ppm of H<sub>2</sub>S at 350 °C resulted in the formation of a

thick ( $\sim 6.6 \mu\text{m}$ ) Pd<sub>4</sub>S corrosion layer which, while exhibiting lower hydrogen atom permeability than pure Pd, retained its catalytic activity for H<sub>2</sub> dissociation. The slow flux decline observed for the Pd foil at longer H<sub>2</sub>S exposure times is consistent with a Pd<sub>4</sub>S corrosion layer that is continually growing. In contrast, the Pd<sub>47</sub>Cu<sub>53</sub> membrane resisted bulk corrosion and sulfur penetrated less than  $\sim 3 \text{ nm}$  into its surface. However, because the hydrogen flux through the alloy membrane was undetectable within 5 min of H<sub>2</sub>S exposure, the thin Pd–Cu–S terminal layer that formed at the top-surface of the alloy must be inactive for hydrogen dissociation or impermeable to hydrogen atoms.

### Acknowledgement

This technical effort was performed in support of the National Energy Technology Laboratory's on-going research in Computational and Basic Sciences under the RDS contract DE-AC26-04NT41817.

### References

- [1] I.B. Elkina, J.H. Meldon, Hydrogen transport in palladium membranes, *Desalination* 147 (2002) 445–448.
- [2] M.V. Mundschau, X. Xie, C.R. Evenson, A.F. Sammells, Dense inorganic membranes for production of hydrogen from methane and coal with carbon dioxide sequestration, *Catal. Today* 118 (2006) 12–23.
- [3] P.M. Thoen, F. Roa, J.D. Way, High flux palladium–copper composite membrane for hydrogen separations, *Desalination* 193 (2006) 224–229.
- [4] L. Yuan, A. Goldbach, H. Xu, Segregation and H<sub>2</sub> transport rate control in body-centered cubic PdCu membranes, *J. Phys. Chem. B* 111 (2007) 10952–10958.
- [5] T.B. Flanagan, D. Wang, K.L. Shanahan, Diffusion of H through Pd membranes: effects of non-ideality, *J. Membr. Sci.* 306 (2007) 66–74.
- [6] H. Amandusson, L.-G. Ekedahl, H. Dannetun, Hydrogen permeation through surface modified Pd and PdAg membranes, *J. Membr. Sci.* 193 (2001) 35–47.
- [7] S.-Y. Liu, Y.-H. Kao, Y. Oliver Su, T.-P. Perng, Analysis of hydrogen and deuterium absorption kinetics in Pd nanofilms, *J. Alloys Compd.* 311 (2000) 283–287.
- [8] H. Li, H. Xu, W. Li, Study of  $n$  value and  $\alpha/\beta$  palladium hydride phase transition within the ultra-thin palladium composite membrane, *J. Membr. Sci.* 324 (2008) 44–49.
- [9] C.H.F. Peden, B.D. Kay, D.W. Goodman, Kinetics of hydrogen absorption by chemically modified Pd(110), *Surf. Sci.* 175 (1986) 215–225.
- [10] F. Gallucci, F. Chiaravalloti, S. Tosti, E. Drioli, A. Basile, The effect of mixture gas on hydrogen permeation through a palladium membrane: experimental study and theoretical approach, *Int. J. Hydrogen Energy* 32 (2007) 1837–1845.
- [11] K. Nobuhara, H. Kasai, W.A. Dino, H. Nakanishi, H<sub>2</sub> dissociative adsorption on Mg, Ti, Ni, Pd and La surfaces, *Surf. Sci.* 566–568 (2004) 703–707.
- [12] B.D. Morreale, B.H. Howard, O. Iyoha, R.M. Enick, C. Ling, D.S. Sholl, Experimental and computational prediction of the hydrogen transport properties of Pd<sub>4</sub>S, *Ind. Eng. Chem. Res.* 46 (2007) 6313–6319.
- [13] B.D. Morreale, The Influence of H<sub>2</sub>S on Palladium and Palladium–Copper Alloy Membranes, *Chemical Engineering*, vol. Doctor of Philosophy, University of Pittsburgh, 2006.
- [14] D.J. Edlund, W.A. Pledger, Thermolysis of hydrogen sulfide in a metal-membrane reactor, *J. Membr. Sci.* 77 (1993) 255–264.
- [15] D.L. McKinley, Metal alloy for hydrogen separation and purification, USA, 1967.
- [16] P. Kamakoti, B.D. Morreale, M.V. Ciocco, B.H. Howard, R.P. Killmeyer, A.V. Cugini, D.S. Sholl, Prediction of hydrogen flux through sulfur-tolerant binary alloy membranes, *Science* 307 (2005) 569–573.
- [17] O. Iyoha, R. Enick, R. Killmeyer, B. Howard, M. Ciocco, B. Morreale, H<sub>2</sub> production from simulated coal syngas containing H<sub>2</sub>S in multi-tubular Pd and 80wt% Pd–20 wt% Cu membrane reactors at 1173 K, *J. Membr. Sci.* 306 (2007) 103–115.
- [18] O. Iyoha, R. Enick, R. Killmeyer, B. Morreale, The influence of hydrogen sulfide-to-hydrogen partial pressure ratio on the sulfidization of Pd and 70 mol% Pd–Cu membranes, *J. Membr. Sci.* 305 (2007) 77–92.
- [19] A. Kulprathipanja, G.O. Alptekin, J.L. Falconer, J.D. Way, Pd and Pd–Cu membranes: inhibition of H<sub>2</sub> permeation by H<sub>2</sub>S, *J. Membr. Sci.* 254 (2005) 49–62.
- [20] D.J. Edlund, Hydrogen-permeable metal membrane and method for producing the same, US Patent 6,152,995 (2000).
- [21] B.H. Howard, R.P. Killmeyer, K.S. Rothenberger, A.V. Cugini, B.D. Morreale, R.M. Enick, F. Bustamante, Hydrogen permeance of palladium–copper alloy membranes over a wide range of temperatures and pressures, *J. Membr. Sci.* 241 (2004) 207–218.
- [22] J.Y. Yang, C. Nishimura, M. Komaki, Effect of H<sub>2</sub>S on hydrogen permeation of Pd<sub>60</sub>Cu<sub>40</sub>/V–15Ni composite membrane, *J. Alloys Compd.* (2007) 446–447.
- [23] F. Roa, J.D. Way, R.L. McCormick, S.N. Paglieri, Preparation, Characterization of Pd–Cu composite membranes for hydrogen separation, *Chem. Eng. J.* 93 (2003) 11–22.
- [24] S. Nam, Y. Seong, J.W. Lee, K. Lee, Preparation of highly stable palladium alloy composite membranes for hydrogen separation, *Desalination* 236 (2009) 51–55.
- [25] D.L. McKinley, Method for hydrogen separation and purification, USA, 1969.
- [26] F. Roa, M.J. Block, J.D. Way, The influence of alloy composition on the H<sub>2</sub> flux of composite Pd–Cu membranes, *Desalination* 147 (2002) 411–416.
- [27] X. Zhang, W. Wang, J. Liu, S. Sheng, G. Xiong, W. Yang, Hydrogen transport through thin palladium–copper alloy composite membranes at low temperatures, *Thin Solid Films* 516 (2008) 1849–1856.
- [28] J.Y. Yang, C. Nishimura, M. Komaki, Hydrogen permeation of Pd<sub>60</sub>Cu<sub>40</sub> alloy covered V–15Ni composite membrane in mixed gases containing H<sub>2</sub>S, *J. Membr. Sci.* 309 (2008) 246–250.
- [29] B.D. Morreale, M.V. Ciocco, B.H. Howard, R.P. Killmeyer, A.V. Cugini, R.M. Enick, Effect of hydrogen–sulfide on the hydrogen permeance of palladium–copper alloys at elevated temperatures, *J. Membr. Sci.* 241 (2004) 219–224.
- [30] L. Yuan, A. Goldbach, H. Xu, Real-time monitoring of metal deposition and segregation phenomena during preparation of PdCu membranes, *J. Membr. Sci.* 322 (2008) 39–45.
- [31] S.M. Opalka, W. Huang, D. Wang, T.B. Flanagan, O.M. Lovvik, S.C. Emerson, Y. She, T.H. Vanderspurt, Hydrogen interactions with the PdCu ordered B2 alloy, *J. Alloys Compd.* 446–447 (2007).
- [32] J.Y. Yang, C. Nishimura, M. Komaki, Effect of overlayer composition on hydrogen permeation of Pd–Cu alloy coated V–15Ni composite membrane, *J. Membr. Sci.* 282 (2006) 337–341.
- [33] P. Kamakoti, D.S. Sholl, A comparison of hydrogen diffusivities in Pd and CuPd alloys using density functional theory, *J. Membr. Sci.* 225 (2003) 145–154.
- [34] P. Kamakoti, D.S. Sholl, Ab initio based lattice gas modeling of interstitial hydrogen diffusion in CuPd alloys, *Phys. Rev. B* 71 (2005).
- [35] R. Ngameni, C. Decaux, D. Solas, S. Grigoriev, P. Millet, Time and frequency domain analysis of hydrogen permeation across PdCu metallic membranes for hydrogen purification, *Int. J. Hydrogen Energy* (2009), doi:10.1016/j.ijhydene.2009.1008.1100.